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MULTI-SALVO GRENADE LAUNCHER ABBREVIATED ANALYSIS

STUDY REPORT

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MULTI-SALVO SMOKE GRENADE LAUNCHER ABBREVIATED ANALYSIS

1. MISSION NEED/THREAT.

- a. Current combat vehicles across the Army are equipped with different smoke grenade launchers that were developed as part of each specific vehicle program. These different launchers all provide the same basic smoke screen capability for the various vehicles on which they are mounted. The need exists to standardize the grenade launchers that will be mounted on all future Army combat vehicles. This will reduce the cost of the launchers and provide for interchangeability from one vehicle to the next. Also, the current launchers do not provide operator selected screening to the front, sides, or overhead. These deficiencies were identified in the 1987 and 1989 Battlefield Deficiency Plan (BDP).
- b. Threat weapon systems utilizing electro-optical, infrared, microwave or radio frequency guidance schemes coupled with target acquisition systems using comparable wavelength sensors greatly increase the lethality of the battlefield. These systems, deployed on a variety of platforms, ranging from manportable to airborne, increase the capability of the threat force to fight effectively under a wide range of battlefield and environmental conditions. Technological advances also offer the potential for threat forces to employ Directed Energy Weapons (DEW). DEW systems (laser, radio frequency, sonic wave, and particle beam) are expected to have a variety of applications to include anti-sensor and anti-vehicular.
- c. The Multi-Salvo Grenade Launcher (MSGL) will launch obscurant grenades to provide the host vehicle with concealment from threat surveillance, target acquisition systems, and weapon guidance systems by placing an obscurant screen between the observation/weapon system and the vehicle. The MSGL will be capable of firing its munitions to the front, sides, or above the vehicle to provide it protection in all directions.

2. ALTERNATIVES.

a. A draft Trade-Off Analysis (TOA) identified and ranked several currently fielded US Army and Allied smoke grenade launchers, along with MSGL as possible candidates to meet the technical characteristics stated in the MSGL Required Operating characteristics (ROC). The MSGL was ranked first, and the currently fielded M257 smoke grenade launcher was ranked second. The M257 was chosen as the base case and the MSGL as the alternative system for this Abbreviated Analysis (AA). Product improvement of the M257 was not included as an alternative because the program cost was estimated to be the same as MSGL, and have a later fielding schedule.



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- b. The M257 is shown in Figure
 1. It consists of four discharger
 tubes and a mounting base with a
 wiring harness and a resistor. The
 M257 is currently mounted on the
 Bradley, and several other combat
 vehicles. The M257 is proposed for
 the M1A2 Abrams (four 4-tube
 launchers) in lieu of the heavier,
 costlier 6-tube, and less efficient
 launchers currently on the M1 and M60
 series tanks.
- The alternative, MSGL, is M257 **GRENADE** Figure 1 shown in Figure 2. It consists of 4 LAUNCHER discharger tubes (identical in function to the M257 tubes) and a mounting base which contains a wiring harness, resistor, and diode. The base is similar to the M257 base, but mounts the discharger tubes with mounting bolts that are accessible from the The bolts on the M257 are accessible only front of the launcher. from the back of the mounting bracket. This MSGL feature provides better maintainability than the M257, in that it can be repaired more quickly. Both the M257 and MSGL are repaired by replacement of individual tubes, and neither launcher assembly is discarded upon failure of tubes.
- Although the wiring of the M257 and the MSGL differ, both launchers can be interfaced with an automatic vehicle firing and testing circuit. However, the wiring of the MSGL permits built-in firing circuit continuity testing, whereas the M257 does not. Also, the built-in test to determine if a launcher tube is loaded with a grenade will allow each of four tubes to be checked with MSGL, versus an aggregate of 4 tubes with M257. BIT with the M257 launcher would indicate that the launcher was loaded with grenades if any of the four tubes contained a grenade. BIT with MSGL

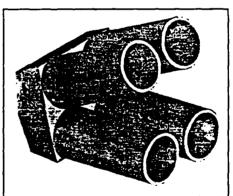


Figure 2 MSGL GRENADE LAUNCHER

would indicate that the loader was loaded only if all four launcher tubes were loaded. This feature would become important if an automatic firing circuit were to be required to switch from an empty launcher to a loaded one with a high degree of confidence that the firing would produce a full 8 grenade salvo of smoke.

e. The interface of the launchers to the vehicles will be a connection of the wiring harnesses of either the MSGL or M257 to

the host vehicle electrical/electronic system. For the HFM/Block III tank, this connection will be made to the vehicle electronics (Vetronics) data/power bus for power and for processing of the launcher firing function by digital signals within the vehicle self defense system logic. Both launchers equally provide a means of connection to the vehicle. Neither launcher circuit provides any additional processing of digital signals to Vetronics.

- f. A salvo of smoke is defined as the firing of a number of grenades to produce a sufficient cloud of smoke for a desired amount of coverage. This has been determined to be 120 degrees around the vehicle. Current grenades provide 15 degrees of smoke each. Therefore, it takes 8 grenades launched 15 degrees apart to produce a cloud of smoke that provides 120 degrees of coverage. MSGL and the M257 launchers both provide a 120 degree smoke cloud.
- g. The four tubes on one MSGL launcher are arranged into two sets of parallel tubes. The parallel sets of two tubes each are 15 degrees apart. Firing two tubes (one from each parallel set) from a launcher provides 30 degrees of coverage around the vehicle. Hence, the smoke of two grenades from four separate MSGL launchers provides a total of 120 degrees coverage, and two salvos of 120 degree coverage without reloading.
- h. All of the four tubes of the M257 launcher are angled 15 degrees apart, which provides 60 degrees of contiguous smoke coverage around the vehicle per launcher. Therefore, two 4-tube M257 launchers fired simultaneously will produce 120 degrees of coverage. Four 4-tube M257 launchers will produce two salvos of 120 degree coverage without reloading.
- i. The smaller angles of the tubes of the MSGL reduces the vehicle surface mounting space required, measured perpendicular to the mounting surface. This smaller space would provide flexibility in location of launchers on any given vehicle. Some flexibility is lost, however, because a single salvo from MSGL launchers would still require the mounting of 4 launchers (16 tubes) at one location on the vehicle, whereas the MC57 would only require two launchers (8 tubes).
- j. Neither the requirement for overhead smoke nor the technical description of an overhead smoke system have been developed. It is therefore impossible to assess the worth of the ability of a launcher to produce overhead smoke. However, it is postulated by CRDEC engineers that because of tube orientation, the MSGL will provide more contiguous overhead smoke coverage than the M257. Testing has not been performed to compare the ability of the launchers to provide overhead coverage. However, since the MSGL Trade Off Analysis listed the MSGL as "excellent" and the M257 as "good" in the capability to produce overhead

smoke, for study purposes, it is assumed that both have some capability.

3. ESSENTIAL ELEMENTS OF ANALYSIS (EEA).

- a. What vehicle application requirements are associated with the performance and physical characteristics of the base case and the MSGL?
- b. What are the applicable Life Cycle Costs (LCC) associated with each performance and physical characteristic of the base case and the MSGL?
- c. What is the range of production quantities of the base case and the MSGL?
- d. How does production quantity affect the unit production cost of the base case and the MSGL over the range of possible production quantities?

4. ANALYSIS OF SYSTEM CHARACTERISTICS, PERFORMANCE AND EFFECTIVENESS.

- a. The purpose of this analysis is to discriminate among the two alternatives where actual differences exist using measures of system characteristics, performance, and effectiveness (CPE). These measures have been derived from engineering estimates of performance, and system descriptions.
- b. In this section the systems will be ranked based upon a quantitative comparison of the physical characteristics of the systems. This comparison is shown in Table 1.

Table 1. Quantitative Comparison

	Base d		MS(Measure	_
Weight (lb)	12	2	11	1
Reliability (MSBF)	49	SAME	49	SAME
Maintainability(MTTR)	1.5	2	1.2	1
Maintenance Manhours Per Year (1000 MH) Army Wide	15.3	2	12.2	1
Single Tube Replaced	YES	SAME	YES	SAME
Mounting Space(sq in)	85	2	58	1

MSBF - Mean Salvo Between Failure

MTTR - Mean Time To Repair (Clock Hours)

Maintenance Manhours Per Year were calculated based on the following:

Maintenance MH Per Year = Failures/Year X MH/Failure; and

Failures/Yr = No. Launchers X Salvos/Yr/Launcher / MSBF

MH/Failure = MTTR X No. of Mechanics per Clock Hour

where: No. Launchers = 100,000 (assumed)

Salvos/Launcher/Yr = 5 (Peacetime estimate by Concepts Br., DCD, USAARMS)

MSBF = 49 Salvos/failure (RAM Rationale)

No. of Mechanics per Clock Hour = 1 (one

man/task)

c. The performance characteristics of the launch tube and the mounting base will be compared in this section. This comparison is shown in Table 2.

Table 2. Launch Tube & Base Comparison

Characteristic	M257	MSGL	HFM ROC	MSGL ROC
Multi salvo	YES	YES	YES	YES
120 DEGREES	YES	YES	YES	YES
240 DEGREES	YES	YES	МО	YES
360 DEGREES	YES	YES	NO	YES
OVERHEAD	YES	YES	NO	YES

d. A comparison of the abilities of the two discharger assemblies to meet the various coverages of smoke could only be made subjectively for the following reasons. First, the host vehicle turret designs have not been finalized. Therefore the total amount of space available for mounting the launchers is not known. Second, the components and technology that will be used in the design of a combat vehicle self defense/countermeasure system have not been defined to the resolution required to determine the number and location of smoke grenade launchers. Smoke grenades are one type of countermeasure technology being considered for the self defense systems. One program proposed is

the Vehicle Integrated Defense System (VIDS). VIDS is being developed by TACOM and is scheduled for proof of principle demonstration in 2Q91 as part of the Component Advanced Technology Test Bed (CATT-B). Smoke grenades will compete with vehicle exhaust produced smoke and other active and passive countermeasure technologies for space, funds, and the weight allowance allocated for the entire vehicle defense system. Once the turret designs are known, and the best mix of smoke and/or other countermeasures have been determined the comparison of the two launchers can be better quantified.

- e. The comparison shown in Table 2 is based on an estimate of the feasibility of mounting 2 assemblies (1 salvo/8 tubes) of either the MSGL or the M257 on the front, and/or sides of a vehicle similar to the M1A1. For smaller vehicles, such as the Bradley, or the "turretless" block III tank it becomes more difficult to mount the same amount of launchers around the vehicle or to provide multiple salvos at one location than on a larger turreted vehicle.
- f. Regardless of the number and location of the grenade launchers finally chosen for the VIDS/self defense system, the total space claimed on the vehicle by the MSGL would be less than the space claimed by the M257. This is because the MSGL has a smaller mounting base and less tube spread than the M257. As the space to mount launchers becomes smaller, or the number of launchers increases, this attribute becomes more important.
- g. The current requirement for the Heavy Force Modernization ROC is for "multiple" salvos of grenade launched smoke, 120 degrees forward of the vehicle. This requirement could be satisfied by two salvos (4 launchers/16 tubes) of either the MSGL or the M257. If the vehicle requirement is later established for greater than 120 degrees of smoke or for an overhead canopy of smoke additional launchers would be required on the vehicle. The smaller mounting space required by the MSGL would facilitate the mounting of additional launchers. Again, depending on the design of the turret (host vehicle) it may be just as easy to mount additional M257 launchers.
- h. The performance characteristics of the circuit for each of the launchers will be compared in this section. This is shown in Table 3.

Table	3.	Launcher	Circuit	Comparison
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Characteristic	M257	MSGL	HFM ROC	MSGL ROC
BIT (continuity)	ио	YES	ИО	YES
BIT (grenade in tube)	4 tubes	each tube	ИО	YES
Automatic Firing	YES	YES	ио	по
VIDS/VETRONICS INTERFACE	YES	YES	YES	YES

5. COST.

a. Introduction. This section presents the detailed results of the Multi-Salvo Grenade Launcher (MSGL) cost analysis to support the MSGL Abbreviated Analysis (AA).

(1) Alternatives.

- (a) The Base Case is a M257 Grenade Launcher Discharger 4 tubes) (NSN 1040-01-095-0091). Figure 3 is a schematic drawing of components of the M257 Grenade Launcher Discharger. It is a hardwire configuration with three subassemblies:
 - Base housing with standard connecting bolt holes to connecting variant vehicle.
 - 2 Four discharger tubes attached to base housing.
- $\underline{3}$ Electrical wire harness and connectors within base housing. Required to fire all four tubes simultaneously.
- (b) Alternative 1 is a Multi-salvo Grenade Launcher (MSGL) Discharger (4 tubes). It is a hardwire configuration with three subassemblies:
- 1 Base housing with standard connecting bolt holes to connecting variant vehicle (slight physical modification to facilitate reduced mounting footprint of turret for host vehicles).

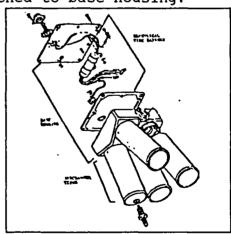


Figure 3 M257 GRENADE DISCHARGER

- $\underline{2}$ Four discharger tubes attached base housing (identical to M257 design for costing).
- 3 Electrical wire harness and connectors within base housing (additional wires included in harness to facilitate increased BIT (continuity) capability and ability to fire individual discharger tube).
- (c) Both the Base Case and Alternative 1 will fire the standard M76 and L8 smoke grenades, as well as the developmental XM81 millimeter screening grenade.
 - (2) Ground Rules.

- (a) All costs prior to FY90 are considered sunk and therefore will not be reflected within LCC Development Costs.
- (b) All costs are presented in current and FY90 constant dollars.
- (c) The operational life of each study alternative is 20 years (identical to appropriate vehicle operational life).
 - (3) Assumptions.
- (a) Production and deployment schedules are identical for Base Case and Alternative 1.
- (b) M257 quantities produced before FY94 will be considered sunk for this cost analysis. Listed below are production quantities of M257 produced since FY 86 (per AMSMC-CAR-S)

	86	87_	88	89	_90_	91	TOTAL
M257 LAUNCHERS	243	600	288	0	0	398	1529
M257 DISCHARGERS	486	1200	576	0	0	796	3058

(c) Quantity requirements for M257 and MSGL from FY94 and later will be identical for the Base Case and Alternative 1. Annex 1 reflects an estimated requirement of 150,000 dischargers for twenty host vehicles within the Army's inventory. The main variables in determining the production requirements are the number of vehicles and number of dischargers per vehicle. These two variables are estimates. Consequently, for this study, it was estimated that dischargers will fall in a range from a minimum of 10,000 to a maximum of 100,000 units to meet proposed production requirements.

- (d) Bradley Fighting Vehicle (BFV) is presently equipped with the M257 and is an adequate representation to formulate a standard vehicle MSGL (vs M257) incremental integration cost.
- b. Methodology. The Life Cycle Cost Estimates (LCCE) and Sensitivity Analysis (SA) focussed on comparisons of Development, Production, Military Construction, Fielding and Sustainment costs of the Base Case and Alternative 1. Cost impact of the reliability, availability, and maintainability (RAM) rationale is incorporated into this cost analysis. In-depth Logistic Impact Analysis (LIA) and Training Analysis (TA) were not conducted in conjunction with this cost analysis.
- (1) LCCE for the Base Case and Alternative 1 were obtained from AMSMC-CAA(A) and AMSMC-CAR-S, and validated at level III. LCCE for each case was provided in "C" matrix format per DCA-P-92(R) and projected at the minimum (10,000) and maximum (100,000) level. AMSMC-CAR-S inputted their data at the 50,000 and 500,000 level. Per AMSMC-CAR-S cost analyst, all LCCE elements can be reduced linearly, less development costs. Chief of Cost, TRAC has reviewed and approved all LCCE for use in this study.
- (2) U.S. Army Armor School (USAARMS) has conducted a cursory review pertaining to host vehicle standard integration cost impact associated with MSGL.
- (3) TRAC-WSMR has reviewed and provided final certification for this cost analysis.
- c. Life Cycle Cost. LCC provided in Table 4 is a summary level presentation of the Life Cycle Cost Estimate (LCCE) for the Base Case and Alternative 1. For a detailed presentation of the LCCE data refer to Annexes 2 through 4. The greatest incremental LCCE cost difference is \$9.2 million associated with the non-sunk Development costs. Production, Fielding, Military Construction, and Sustainment cost elements are the remaining LCCE cost differentials. All of these cost categories will be discussed in detail in the following paragraphs.

Table 4. Summary of Submitted Life Cycle Costs

(FY 90 CONSTANT DOLLARS IN MILLIONS)

		257 CASE	MSGL ALT. 1		INCREM MSGL VS	
PRODUCTION QTY	10,000	100,000	10,000	100,000	10,000	100,000
DEVELOPMENT	0.0	0.0	9.2	9.2	+ 9.2	+ 9.2
PRODUCTION	1.34	12.81	1.67	12.56	+ 0.33	(0.25)
MILITARY CONSTRUCTION	0.0	0.0	0.0	0.0	0.0	0.0
FIELDING	0.04	0.4	0.05	0.45	+ 0.01	+ 0.05
SUSTAINMENT	<u>.55</u>	5.5	0.02	0 <u>.15</u>	(0.53)	(5.35)
TOTAL LCC	1.93	18.71	10.94	22.36	+ 9.01	+ 3.65

(1) Development Costs. The major cost differences between the Base Case and Alternative 1 occurs within the Development LCCE. Alternative 1 development costs represent over 80% of the total LCCE incremental cost. Table 5 reflects the total \$14.5 million Development costs and incremental non-sunk \$9.2 million developmental costs requirements for the MSGL program.

Table 5. MSGL Time-Phased Development Costs.

(FY 90 CONSTANT DOLLARS IN MILLIONS)

SUNK	FY 91	FY 92	FY 93	FY 94	TOTAL
5.269	3.626	3.491	2.092	0.0	14.478

- (a) The \$9.2 million non-sunk development costs represents the Full Scale Development(FSD) Phase of MSGL for a varied number of type host vehicles. A total of 1332 MSGL dischargers are expected to be fabricated during FSD to accommodate test requirements. Unit cost of prototype is \$200.
- (b) It should be noted that the development funds reflected above are for a semi-smart (digital) MSGL as stated in the present MSGL Baseline Cost Estimate (BCE). During the proof

of principle phase it was decided that the most cost effective method was to provide a hardwire circuit design MSGL and utilize the smart digital capability (1553 bus) within the host vehicle. However, PM-Smoke has verbally indicated the non-sunk development funds reflected will be required for either a hardwire or digital MSGL.

(2) Production Costs. Table 6 reflects the Production Recurring (manufacturing) cost is the most significant Production incremental cost. LCCE recurring costs for the Base Case reflect a constant Average Unit Cost (AUC) compared to a variable AUC within Alternative 1. As stated above, the present MSGL BCE and submitted recurring Production LCCE (shown in annex 3) reflects a higher cost semi-smart (digital) MSGL that is not a viable option. Consequently, the validated XM6 MSGL discharger with a variable manufacturing cost, as shown in Annex 4, is utilized as the recurring production cost for Alternative 1. remaining submitted Production LCCE elements (engineering support, training devices and other elements) for all cases have not been altered and are not significant cost drivers for detailed analysis. However, as stated previously in the study, the present M257 procurement level since FY86 has been at a very reduced level and in order to ramp up for the 100,000 procurement level engineering support, training devices and other elements for the M257 should be identical to the MSGL LCCE level.

Table 6. Submitted LCCE Production Costs
(FY 90 CONSTANT DOLLARS IN MILLIONS)

-		257 CASE	MSGI ALT			EMENTAL /S M257
PRODUCTION QTY	10,000	100,000	10,000	100,000	10,000	100,000
NON-RECURRING	0.0	0.0	0.0	0.0	0.0	0.0
RECURRING	1.27	12.74	1.59	11.91	+ 0.32	(0.83)
RECURRING ENG.	0.07	0.07	0.03	0.25	(0.04)	+0.18
TRAINING DEVICES	0.0	0.0	0.0	0.02	0.0	+ 0.02
OTHER	0.0	0.0	0.05	0.5	+_0.05	+ 0.5
TOTAL LCC	1.34	12.81	1.67	12.68	+ 0.33	(0.13)

(a) Sensitivity Analysis of Recurring Production Costs. The <u>cost/quantity</u> relationship (Economies of Scale) of the M257 and MSGL discharger is explored in detail. Below is a

detailed breakdown of elements that make-up the MSGL manufacturing cost at both the 10,000 and 100,000 production levels provided by CRDEC. This elemental breakdown clearly demonstrates the lower unit cost/increase quantity relationship associated with decreased unit cost of materials, better utilization of management, and decreased unit cost of labor through dilution of fix costs (overhead).

XM6 MSGL Design to Unit Production Unit Cost(DTUPC) - Data from Annex 4

			100,000				
		\$	\$/unit	*	\$	\$/unit	
1.	MFG. LABOR	523483	52.35	33	3696623	36.97	31
2.	PARTS MATERIAL	640752	64.08	43	5348280	53.48	45
3.	ENGR. and SUPPORT	84531	8.45	5	291505	2.92	3
4.	G & A (std %)	212290	21.23	抖	1587189	15.87	13
5.	PROFIT (std %)	131495	13.15	8	983124	9.83	8
	TOTAL	159255 2	159.26	100	11906721	119.07	100

(b) Variable M257 Production. Conversely, due to time

constraints the M257 discharger DTUPC submitted for the 10,000 and 100,000 manufacturing cost reflected a constant \$127. This constant DTUPC has been reflected in all LCCE production cost data for the M257. However, the reduced lower DTUPC cost/increased quantity logic should apply to the higher production level of the M257 case. Figure 4 is a graphical representation of both the M257 and MSGL unit production costs. For the MSGL variable production levels a variable \$159/\$119 DTUPC is reflected in the cost data. For the

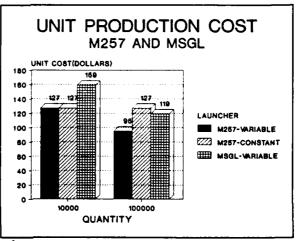


Figure 4 UNIT COST

M257 variable production levels a <u>constant \$127 DTUPC</u> is reflected in the original cost data. The solid black bar depicts a M257 <u>variable \$127/\$95 DTUPC</u> which is in relationship to the MSGL variable DTUPC (\$159/\$119). Consequently, for comparison

purposes, the variable M257 DTUPC is a more representative unit production cost than the constant DTUPC and will be used in this cost analysis.

- (3) Military Construction. No military construction is required to support the MSGL improvements.
- (4) Fielding. Referring back to Table 4 the fielding LCC of the MSGL alternative appears greater than Base Case. This is mainly attributable to the advanced and normal fielding of initial spares to fill the pipeline of a new commodity. Below is Table 7 which is a breakdown of the fielding LCCE elements:

Table 7 Submitted LCCE Fielding Costs (FY 90 Constant Dollars in Million)

		MSGL ALT. 1		
10,000	100,000	10,000	100,000	
0.0	0.0	.04	0.4	
04_	0.4	01	0.1	
.04	. 4	.05	0.5	
	10,000 0.0 .04	0.0 0.0	BASE CASE ALT 10,000 100,000 10,000 0.0 0.0 .04 .04 0.4 .01	

- Sensitivity Analysis of Initial Repair Parts. AMSSMC-CAR-S assumed there will be no requirement for initial spares for the MSGL discharger since only five component parts (out of a total of 27 component parts) are within the logistic system and those five are common to other weapon systems. In contrast, AMSMC-CAA reflected a maximum of \$400,000 for initial repair parts to facilitate the higher volume ramp up requirements for the MSGL (Army's projected standard discharger for approximately twenty different host vehicles). As stated earlier, the present acquisition requirements experienced for the M257 have been procured in small lot sizes (for a minimum number of host vehicles) minimizing the need for a formal ramp up. However, for both M257 and MSGL high volume levels, it is subjectively concluded that projected ramp up requirements will necessitate an advance and normal fielding of repair parts. Consequently, a maximum of \$400,000 of initial repair parts is required for both the M257 and MSGL high volume cases.
- (b) Sensitivity Analysis of First Destination Transportation Costs (FDTC). The incremental increase is associated with the M257 and the details that support this increase are reflected in Annex 5. In summary, the M257 is

produced in New York State and FDTC (\$3.83/ discharger) is based on shipments from producer to Letterkenny Army Depot. Conversely, the present MSGL LCC FDTC is one-fourth of the M257. Per TRADOC/FORSCOM Cost Planning Factors, transportation cost is based on cost per ton mile. As stated earlier, the weight of M257 and MSGL only differ by one pound. Thus, the number of miles transported is the main variable for any cost difference between the M257 and MSGL. Present vendor selection process has not taken place for MSGL to identify with assurance transportation distance. Consequently, at this stage, it would be more prudent to utilize the higher and more defined M257 FDTC for all cases, reflecting equal costs for both systems.

- (5) Sustainment. Referring back to Table 4 the sustainment cost in all cases relates only to the OMA funds associated with the replenishment of repair parts managed by The LCCE supports the concept reflected in the technical manual which indicates that the components are very durable and maintenance free. For both the Base Case and MSGL Alternative the discharger design is simple and sustainment effort is reduced to replacing expendable parts, as required, to operate and maintain the discharger. There is no ASL/PLL for either system and all repairs are completed at the unit/organization level. There are no depot repairs. The minimum engineering changes associated with MSGL minimizes any sustainment cost differences. The significant difference reflected in the LCCE submitted is mainly associated with the number of years sustainment was reflected between the Base Case and Alternative 1. The projected LCC for the Base Case was based on 20 year life/20 years of replenishment (see annex 2). Alternative 1 was based on 15 year life/8 years of replenishment (per Cost Analyst at AMSMC-CAA). Replenishment costs for Alternative 1 are also based on a semismart MSGL.
- (a) Sensitivity Analysis of Replenishment Repair Parts (RRP). AMSMC-CAR-S provided in-depth data describing the method utilized to develop M257 RRP costs. The RRP costs were estimated by multiplying the number of active M257 dischargers by the failure factor for a particular part and then multiplying the contract price of the part inflated to FY 90 constant dollars. The fielded M257 dischargers rate of 94% was arrived at by an activity rate of 95% (AMSMC-CAR assumption) minus 1% maintenance float (failure factor of discharger is 1%). On the next page is a summation of data reflected in Annex 6 which provides a roll-up of the inputted LCC RRP.

			BASE CASE	M257
			10,000	100,000
Gasket Tube Elect contact Resistor Cap plug	= =	2.7 % 5.3 % 6.2 % 6.1 % 79.7 %	\$ 455,274	\$ 4,552,743
Total		100 %	\$ 555,461	\$ 5,555,461
Less cap plug		20.3 %	\$ 111,092	\$ 1,110,920

2 According to the smoke grenade technical manual (reference 12) the cap plug is not a component of the M257 discharger but a component of the M257 Launcher (which consists of two dischargers plus eight cap plugs) and thus should not have been reflected in the AMSMC-CAR-S LCC RRP analysis. For all cases the cap plug will require removal before arming the discharger and thereby will not reflect any cost differential in usage or RRP consumption. Removing the cap plug cost impact of the RRP analysis reduces the RRP by 79.7% (\$111,092/\$1,110,920 respectively) as illustrated above. As mentioned above, Alternative 1 submitted RRP was based on 15 year life/8 years of RRP. Below is a simple representation depicting Alternative 1 on a equal basis with the Base Case (20 year life/20 years of RRP).

	Alternat	tive 1 MSGL
	10,000	100,000
Submitted LCCE 15 yr.life/8 yr. RRP	\$20,000	\$150,000
20 yr.life/20 yr.RRP	\$37,500	\$375,000

3 A cursory review will reflect that the M257 RRP is an estimated 8.75% of the LCCE recurring production cost. The MSGL RRP is an estimated 2% to 3% of the LCC recurring production cost. The \$37,500/\$375,000 case indicates reduced failure factors for components of the MSGL discharger. However, the submitted RRP LCCE is based on a semi-smart MSGL with significant lower failure factors. But, the revised MSGL reflects minimum component changes to justify a 6% to 7% reduction in RRP costs. Subsequently, RRP differences for the M257 and MSGL should be based on no changes in recurring cost and the failure factors should be constant for all cases. Utilizing the Base Case 20 year standard percentage of recurring production (8.75%) for all cases is more appropriate than indicating a significant reduction for the MSGL cases.

- (b) RAM Impact on Sustainment Costs. Elements of the RAM analysis are still being developed. However, MTTR, the main emerging cost impact from the RAM analysis has been incorporated within this study.
- (c) Maintainability (MTTR). MTTR is the only RAM improvement that has been quantified reflecting a 3000 direct manhour/year savings (60,000 manhours for twenty years) throughout the Army at the 100,000 procurement level for Alternative 1. This manhour savings is at unit/organization level and distributed over numerous units within the Army, minimizing any impact on reductions to personnel staffing. However, it does indicate a potential cost avoidance in decreasing unit operating resource support requirements and will have a positive impact within the force. Based on TRADOC/FORSCOM Cost Planning Factors (E7 cost is approximately \$25.00/direct hour) the MTTR manhours improvement represents, in monies, an equivalent cost impact of \$75,000/year (\$1.5 million for twenty years).
- d. Sensitivity Analysis (SA) Impact to Life Cycle Costs (LCC). Purpose of the SA is to quantify and refine the submitted LCCE in accordance with the study plan and standardize cost data between alternatives. The SA diverges from the submitted LCC in the following ways.
- (1) Production Cost Recurring. A variable M257 AUC of \$95 vs constant \$127 was utilized for the M257 Base Case higher production level (100,000) case. The resultant reduced the submitted Production LCCE from \$12.81 million to \$9.64 million.
- (2) Production Cost Recurring Eng., Training Devices, and Other Production Costs. Increase M257 10,000 and 100,000 production level cases to reflect identical ramp up cost requirements of MSGL 10,000 and 100,000 Cases. The resultant will increase both M257 cases by \$.07/.58 million respectively.
- (3) Fielding Initial Repair Parts. For ramp up purpose reflect identical costs for all cases. The resultant will increase the M257 cases by \$.04/\$.4 million respectively.
- (4) Fielding First Destination Transportation Costs. Reflect identical costs for all cases. The resultant will increase the MSGL cases by \$.03/\$.3 million respectively.
- (5) Sustainment Replenishment Repair Parts. Utilize the M257 adjusted replenishment standard (less cap plugs) of 8.75% of recurring production for all cases. The resultant will

decrease the M257 cases by \$.44/\$3.37 million respectively and increase the MSGL cases by \$.11/\$.85 million respectively.

Table 8 presents a summary of the SA impact for the Base Case and Alternative 1.

Table 8. Summary of Sensitivity Analysis Impact to LCC

(FY 90 CONSTANT DOLLARS IN MILLIONS)

	=	1257 CASE	MSGL ALT. 1		INCREME MSGL VS M	
PRODUCTION QTY	10,000	100,000	10,000 1	00,000	10,000 10	0,000
DEVELOPMENT	0.0	0.0	9.2	9.2	+ 9.2 +	9.2
PRODUCTION	1.35	10.27	1.67	12.68	+ 0.32 +	2.41
MILITARY CONSTRUCTION	0.0	0.0	0.0	0.0	0.0	0.0
FIELDING	0.08	0.8	0.08	0.8	0.0	0.0
SUSTAINMENT	11	0.83	0.13	1.0	+ 0.02 +	0.17
TOTAL LCC	1.54	11.90	11.08	23.68	+ 9.54	+11.78

e. Integration Cost Impact. Presently the M257 is deployed on the Bradley Fighting Vehicle (BFV). Thus, the BFV is utilized to reflect the possible integration cost differences of M257 vs MSGL.

⁽¹⁾ The BFV technical manual indicates that one M257 launcher (two dischargers/eight tubes) is controlled by the Weapons Control Box (see annex 7) which also controls three other weapon systems (TOW, Coax, and 25mm Chain Gun). Within the operation mode all eight discharger tubes are fired simultaneously. Per CRDEC the MSGL can be adapted to the present BFV and will operate identically to the M257. For future BFV systems the Weapons Control Box will be replaced by a more sophisticated VIDS controller (HFM) system tied to the BFV 1553 BUS. The M257-VIDS configuration will be able to fire each discharger (four tubes) individually. The VIDS/MSGL configuration will have increased capability to fire each discharger tube individually and/or simultaneously. MSGL circuit design will permit individual tube testing and grenade readiness check.

(2) The technical manual defines six possible maintenance fault symptom tests by 45T MOS to perform within the weapons control box/M257 configuration. For future HFM variants the VIDS/MSGL or M257 configuration will most likely reduce 45T MOS manhours in performing these checks. However, it appears the manhours saved will be directly associated with the VIDS capabilities rather than the dischargers. Estimated recurring production cost per unit (below) indicate all future HFM systems integration value is being incorporated into the VIDS. Neither the MSGL nor M257 added cost is significant when compared to the VIDS controller cost.

Present BFV		Future BFV	
Four M257	\$508	Four M257	\$508
Wpns Cntrl. Box	\$1030	VIDS	\$50,000
<u>or</u>		<u>or</u>	
Four MSGL	\$636	Four MSGL	\$636
Wpns.Cntrl.Box	\$1030	VIDS	\$50,000

f. Cost Summary.

- (1) MSGL largest incremental cost is \$9.2 million nonsunk Development costs (approximately 80% of LCC) that represent required Full Scale Development Phase.
- (2) MSGL Recurring production costs are incrementally higher for both low volume buy (10,000) and high volume buy (100,000). DTUPC:

M	<u> [257 </u>	MSGI	<u> </u>
10,000	100,000	10,000	100,000
\$127	\$95	\$159	\$119

- (3) At 100,000 production level, MSGL (vs M257) maintainability (MTTR) reflects a potential cost avoidance in decreasing Army's unit operating support resource requirements by 3000 direct manhours per year (60,000 manhours for twenty years). Equivalent cost impact of \$75,000 per year (\$1.5 million for twenty years) (not included in LCC).
- (4) Based on BFV, vehicle Integration cost impact difference between the M257 and MSGL is minimum.
- 6. GROWTH POTENTIAL COMPARISON. The above comparison of the characteristics of the M257 and MSGL to the current HFM requirements was based on current knowledge of the vehicle and vehicle defense system characteristics. It is possible that these requirements with respect to vehicle smoke will change as the HFM program matures and the self defense systems and vehicle

configurations are further defined. The additional characteristics provided by MSGL will accommodate potential growth in sophistication of the vehicle self-defense systems better than the M257.

7. SUMMARY.

a. System Comparison.

- (1) Quantitative Comparison. The only difference in the alternatives (M257 and MSGL) is in weight, maintainability, and mounting space per launcher. The difference in weight is one pound per launcher. This is an insignificant amount when compared to the total vehicle weight. The difference in footprint size per launcher is equivalent to 9.2 by 9.2 inches for the M257 and 7.62 by 7.62 inches for the MSGL. This may be significant depending upon the vehicle design and number of launchers desired to be mounted on each vehicle.
- (2) Launch Tube and Base Comparison. Of the launch tube and base characteristics in Table 2, there is no quantifiable benefit associated with MSGL. There is a postulated, but unproven benefit of providing overhead smoke with MSGL versus M257. However, there is no current requirement for overhead smoke in the HFM ROC.
- (3) Launcher Circuit Comparison. The launcher circuit of the MSGL provides better BIT capability than the M257. In general, better BIT is a benefit for maintenance. This would not warrant redesign of the launchers. There is no HFM vehicle, or HFM vehicle self defense system requirement established by which the benefit of the improved BIT can be estimated. Should the smoke grenade launchers of HFM, M1 Block III, or M2/3 Block III eventually be required to contain BIT of individual tube and be fired by individual tube, only the MSGL would meet requirements.

b. Discussion.

- (1) The MSGL provides an improvement in the following:
- (a) Maintainability (MTTR).
- (b) Mounting space per launcher.
- (c) Improved BIT.
- (2) Of the above, maintainability is the only characteristic for which a benefit can be determined. By itself, the improvement in maintainability does not justify the incremental LCC of MSGL over the M257. However, the potential cost avoidance due to maintainability of MSGL is substantial when compared to the incremental LCC of MSGL.

(3) The performance benefits ascribed to the MSGL are minimal based on this analysis. Where performance differentials can be measured (BIT and mounting space), there are currently no host vehicle or vehicle self-defense requirements documentation to support such an enhancement. Based on this analysis the MSGL does not provide any benefit over the M257 which would warrant the expenditure of 9 to 12 million dollars at this time.

8. CONCLUSION.

- a. The MSGL will provide a marginal increase in performance over the M257. At a cost of an additional 9 to 12 million dollars the MSGL will provide an improvement in maintainability, mounting space, and improved BIT. On the other hand, MSGL may be necessary to accommodate growth in the sophistication of HFM vehicle smoke systems.
- b. The M257 meets all current HFM vehicle requirements. There is a risk that the M257 will not meet all future HFM design requirements, because smoke grenade launcher technical characteristics are being defined much earlier than the HFM vehicle technical characteristics.

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ANNEXES

- Annex 1 Estimated Production Quantities Requirements
- Annex 2 Base Case Submitted LCCE
- Annex 3 Alternate I Submitted LCCE
- Annex 4 Alternate I Revised Recurring Production Costs
- Annex 5 First Destination Transportation Data
- Annex 6 Replenishment of Repair Parts Data
- Annex 7 BFV Integration Data

ANNEX 1 M257 or MSGL DISCHARGERS ESTIMATED PRODUCTION REQUIREMENTS

(FY 94 - FY06)

1. HFM PACKAGE I (FOUR DISHARGERS/VEHICLE) (DATA FROM HFM COEA)

	# VEHICLES	# DISCHARGERS
BLOCK III/HFM TANK CMV FIFV AFAS LOS-AT FARV-A	3349 249 1893 888 1404 888	13396 996 7572 0 5616 3352
	SUB-TOTAL	30932

2. REMAINDING HFM VARIANTS (FOUR DISCHARGERS/VEHICLE) (DATA TAKEN FROM AFV TOA (CFF)

		+	# VEHICLES	# DISCHARGERS
FRV		•	2000	8000
CGV			612	2448
SAPPER			2134	8536
FSCLOS			934	3736
LOSAD			729	2916
RV			1964	7856
MARS			1967	7868
AA			1484	5936
DEW-V			179	716
FARV-A	* ROUGH ESTIM	ATE	* 2500	10000
FARV-F			* 2500	10000
		SUB-TOTAL		68012

3. ADDITIONAL VARIANTS (12 DISCHARGERS/VEHICLE)

ARMORED SECURITY VEHICLE NBC RECON VEHICLE LARGE AREA SMOKE SCREEN VEHICLE	# VEHICLES 3325 650 508	# DISCHARGERS 39900 7800 6096
		53796
· GRAND	TOTAL	152740

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NNEX 3-- Alternate I - Submitted LCCI

ANNEX 4 - Alternate I Revised Recurring Production Data

IMS Discharger Manufacturing Cost Estimate

23 June 1989

QUANTITY UNIT COST	10,000 \$159.26	100.0 \$119		·	مند	eji.
	x .	5 per 10000	OE	Total	Unit	1
Engr & Spt Mig	117 200	38954.71 174494.5	45577.00 348989.00	84531.71 523483.50	8.45 52.35	3 33
Parts	5	610240	30512.00	840752.00	64.08	40
GLA	17		<u>-</u>	1248767.21 212290.43		13
Profit	9		·	1461057.64		8
TOTAL				1592552,82		-0150.26 each
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Ingr & Spt	117 200	134334 1232208	157171 2464415	291505 3696623	2.92 36.97	2.4 31
Parts	5	5093800	254680	5348280	53.48	45
GŁA	- 17			9336408 1587189		13
Profit	9		ĺ	10923597 983124		8
TOTAL				11006721		\$119.07 each

Projected manufacture of 10,000 or 100,000 dischargers.

Discharger is the "Hardwired" model developed by the AAI Corp. during FT89

Manufacturing time estimates and material costs were taken from:

Contract Report, AAI Corp., Contract DAAA15-85-D-0021 (Task 11),

Sequence No. A047, Data Item: DI-A-5345/T, subj: Design To Cost Report

For The Multi-Salvo Grenade Launcher

Contractor cost data was obtained from:

DF, AMCCOM, AMSMC-CAA (A), 27 Mar 89, subj: FT89 Average Contractor Rates

CONTROL NO: 91027 LEVEL NO: 12

AUTOVONISTY SYTO DATE 3/WE
VALIDATOR 2411 APPROVED BY: 4

VOID AFTER: 23 JUN 90

	E.	z/1,000	Ers/4,000 Tube (4 each)	Ers/40,000	Era/400,000		••••
PARTS			1:40	, 10K	2 100 K	E.	
Cost # total per uni	t	12000 24	20000 20	160000 16	140000 14.00		·
	•						
LABOR	late s/hr		•				
MANUFACTURING				•	•		
Elec Fab	8.50			•			
Riec TstaTool	12.55			•			
Ascembly	8.50		· ·				
Pack & Ship	8.50						
Prod Ctrl	12.65	•					
Elec Prod	8.50		• • • •				
Prod Mgr	12.65				•		
nspection	12.65	• • •	<u> </u>				
A Ingr	10.30						
tecv. Insp	12.65						
•							-
	Cost &	0.	.00 0.0	0 0.	.00	0.00	
IZOINEERI 10			•		0	0	
ir System, I	10.30						
System, I	12.15			•			
lr System	19.30		•				
lysien	12.15					a	70237 NUN 18
roj Mt	29.65					7"	38 33
roj Main	11.05						The same of the sa
LABOR				••	**	£	
	Cost 8	0.	0.0	0 0.	00	0.00	
		•			0	0	·

LABOR and PARTS	(3)		**==+**			K		X	
PARTS		824/300 سوست		Ers/1,0 Base (1	eachi	Brs/10,		Ers/100	
Cost & total		3317		-	<u>~</u>		N K	÷ 10	OK
per unit	ı		_	3691		40194		331760	
Matl # total		33	ع بدين ع	36.9 106		40.10		33.17	
per unit		1.06	;	1.00		1030		7500	
LABOR	late \$/hr			4.40	•	. I.O.	3	0.7	1
MANUFACTURING	*********		•		•				
Riec Fab	8.50	793 1,586		1481		6000	51000	35000	297500
Rice TataTool	19.85	231 0.461	2922.15	1.481	5844.3	-	44275	0.35	
Accembly	8.50	420		0.462 840		6000 6.35		0.2	
Pack & Ship	3.50	0.84 12		0.84 24		0.6		50000	
Prod Cirl	12.65	0.02± 80	832.5	0.024		0.01 300	••••	1000 0.01	
Elec Prod	8.50	0.1 36	308	0.095	344	0.03 200		2000 0.03	20000
Prod Kgr	12.65	0.072 130	1644.5	0.084 224	2833.8	0.02	5060	10000 0.1 400	85000 5060
Inspection	12.65	0.28 75	948.75	0.224 143	1808.95	0.04	1012	0.004 950	12017.3
QL Eafr	19.30	0.15	77.2	0.143	135.1	0.008	388	0.0095	1930
keer. lasp	12.45	0.008		0.007 0	6	0.002	٥	0.001	1930
		0	*	0		0		Ó	•
Enginkering	Cost s		16944		32313	. •	159928 15.9928		1113308
Sr System, I	10.30	350	6735	400	7720	***			
System, I	12.15	0.7 690	8363.5	9.4	8720	400 0.94 800	7720	0.004	7720
Se System	10.30	1.38 390	7527	0.8 473	9167.5	0.0E 400	9720	8500 0.085	103273
System :	12.15		0416.25	0.475 950	11542.5	0.04 950	7720	400	7729
Proj Kji	29.65	1155 40	1186	9.95 40	1186	0.005	11542.5	0.01	12150
Proj Maia	11.95	0.0 8 30	358.5	0.04 40	478	0.004 50	1166 597.5	40 0.0004 100	1186
	•	0.08	~~~~~	0.04	•••••	0.005		0.001	1195
	Cost #		33626	, -	20914.	•	38484 3.8486	•	133246 1.33246

LABOR and PARTS ((4)	•			•	٦	ŧ	*	
7A775	I	18/500 چس	1	Ers/1,000 Discharfer		•	.000 K		00 0 人 2
Katl # total per unit	i	540 1.08		1.08		6000 0.5		40000 0.4	
LABOR	Late S/hr								
MANUFACTURING	:				·				
Elec Fab	8.50								
Elec TataTool	12.65								
Assembly	8,50	65	552.5	130 -	1105	1200	10200	11000	93500
Pack & Ship	8.50	0.13	170	0.13 40	340	0.12 350	2975	0.11 1500	12750
Prod Ctrl	12.65	0.04		0.04		0.035		0.015	
Ilec Prod	8.50								
Prod Mgr	12.65								
Inspection	12.65	6	75.9	12	151.8	110	1591.5	1000	12650
gr gra 16	19.30	0.013		0.012		0.011		0.01	•
Becv. Insp	12.65			į		•			
	Cost 8	•	798		1597	•	14567	•	118900
Enginkebing							1.45665		1.189
Se System, I	19.30								
System, I	12.15				•				
Sr System	19.30	1	38.6	4	77.2	· 10	193	10	193.00
System	. 12.15	0.004		0.004 12 0.012		0.001 20	243	0.0001	850.50
Proj Kgt	29.65		20.755	0.012 0.7	20.755	0.7	20.755	0.7	20.76
Proj Admin		0.0014 0.4	4.78	0.0007 0.5		0.00007	11.05	9.000007 2	23.90
	: ·.	0.0008	*=	0.0008		0.0001			
• •	Cost #		137.04	•	250.93		468.71 0.046870		1088.18 0.010461

PARTS COST							Y -{	•	τ
	per discharger		00.	1,()00'	10,00	0.	100	,000
Cap	4	1.00	4.00	1.00	4.00 -	0.800	3.20	0.650	2.50
Tube	4	5.00	24.00	5.00	20.00	4.000	16.do	3.500	-14.00
ECT	4	5.00	20.00	4.00	16.00	3.500	14.00	3.000	12.00
Base	. 1	15.00	15.00	12.00	12.00	8.000	8.QD	6.000	8.00
lasul. Side	4	0.17	88.0	0.15	0.60	0.100	6. 4	0.080	0.32
lasul. Ind	4	0.07	0.28	0.05	0.20	9.050	0.2D	0.040	0.15
lcrew .	12	0.05	0.60	0.03	0.36	0.030	0.38	0.028	0.34
Jesher	12	0.05	0.60	0.03	0.36	0.030	0.38	0.028	0.34
Screw	4	0.01	0.04	0.01	0.02	800.0	0.03	0.008	0.03
Masher	4	0.0l	0.04	0.01	0.02	9.008	0.03	0.008	0.03
Potting	· 1	3.00	2.00	2.00	2.00	2.000	2.00	1.900	1.90
lastet	1	3.75	3.75	3.60	3.60	1.350	1.35	0.850	0.85
POTAL-Base Pa	rts	****.	42.99		35.16	•	26.75		21.97
Connector	1	4.95	4,05	4.10	4.10	3.250	3.25	3.000	3.00
Resistor	4	0.53	2.12	0.51	2.04	0.350	1.40	0.250	1.00
Diode	4	3.20	12.80	3.10	12.40	1.600	7.25	1.500	6.00
lackpost	2	0.22	0.44	0.20	0.40	0.100	0.25	0.090	0.18
Gasket	1	0.89	0.89	0.85	0.65	0.450	0.45	0.200	0.20
ferminal, Fla	.t 4	0.32	1.28	0.28	1.12	0.080	0.32	0.075	0.30
ferminal Lug	4	0.10	0.40	0.10	0.40	0.100	0.45	0.090	0.36
Mire, 20 AWG	1	0.04	0.04	0.04	0.04	0.040	0.0	0.025	0.03
Mire, 10 1NG	1	0.04	0.04	0.04	0.04	0.040	0.0	0.025	0.03
Solder		·	0.00		0.00	0.000	0.00	0.000	0.00
Turet	1	0.05	0.40	0.05	0.36	0.020	0.1	0.015	0.12
TOTAL-Base El	ect.		25.56	. •	21.75	•	13.48		11.21
707AL for 849	ı		. 66.35		56.01		40.19		33.1%
TOTAL for Dis	cherfer		94.35		80.91		50.30		19.776

A D 3 3 7 JUN 1889

4-6

ANNEX 5 - First Destination Transportation Data

COST DATA RATIONALE

. WORK ELEMENT: First Destination Trans.

COST ELEMENT/CELL:4.031

ITEM: M257 Discharger

DATE: July 1989

COST DATA EXPRESSION:

INCLUDES:

EXCLUDES:

FINAL COST MODEL EXPRESSION:

FY90 CONSTANT (\$000) DOLLARS

. ••	FY91	FY92	FY93	FY94	FY95	FY96	FY97	FY98
QTY/150	8.33	8.33	8.33	8.33	8.33	8.33	8.33	8.33
X \$574	\$ 574	# 574	\$ 574					
First Dest	\$4.8	\$4.8	\$4.8	\$4.8	\$4.8	\$4.8	\$4.8	\$4.8
Transport							j	

SOURCE:

- 1. Transportation Costs from AMSMC-TMR, Fonecon 11 July 1989. Each drum contains 150 dischargers: 1250 / 150 = 8.33 drums/yr. Shipping cost per drum = \$554 x 1.036 = \$573.94 = \$574 (rounded) OSD/OMB Inflation Guidance, dated 22 Dec 88: OMA FY89-FY90=1.036.
- 2. Current Producer is in New York State and Launchers are currently shipped to Letterkenny AD. Source: AMSMC-PDA-D.

: [

ANNEX 6 - Replenishment of Repair Parts Data

VARIABLE/FACTOR RATIONALE

ITEM: Replenishment Repair Parts

VARIABLE: N/A
COST ELEMENT/CELL: 5.011

DATE: July 1989

CURRENT VALUE BEING USED:

See attached detail sheet

DESCRIPTION OF HOW VALUE DERIVED:

- 1. Failure factors were taken from the Y95 report from the NSN-MDR file.
 These factors represent failures per 100 end items. Since the end
 item in this case is the M257 launcher, the failure factors were
 adjusted to reflect the fact that I launcher consists of 2 dischargers.
 (SOURCE: AMSMC-MMN-C)
- 2. Unit contract prices were also taken from the Y95 report from the NSN-MDR (Master Data Record) file.
- 3. The failure factor for the discharger is 2/100 launchers or 2/200 dischargers. This is a failure factor of .01 or 1%. This 1% was used to determine the maintenance float for the discharger.
- 4. An activity rate of 95% was assumed. (SOURCE: AMSMC-CAR assumption).
- '5. The activity rate and the maintenance float was used to determine the fielded quantities: 95% 1% = 94% of production is fielded.
- 6. Only five repair parts are managed by AMCCOM:

NSN	NOMENCLATURE	FF/LAUNCHER	FF/DISCHARGER	UNIT COST
5330-01-096-4551	Gasket	1/100=.01	1/200 = .005	\$1.50
1010-01-246-9930	Tube	1/100=.01	1/200 = .005	\$39.74**
5999-01-096-2017	Contact	3/100=.03	3/200 = .015	\$11.38
5905-01-094-9838	Resistor	1/100=.01	1/200 = .005	\$ 33.89
5340-01-095-0297	Cap-Plug	494/100=4.94	494/200=2.47	\$0.91
1040-01-095-0091	Discharger	2/100=.02	2/200 = .01	\$118.18

- ** This price is the AMDF price for the item which this NSN will replace. Because present stock levels are adequate for the anticipated requirements the replacement part has never been purchased.
- 7. The unit prices were adjusted to FY90 constant dollars by multiplying by the appropriate inflation factor, except in the case of the tube. It was estimated that the AMDF price for ASF items is about 30% higher than the contract price. Hence the tube price was divided by 1.3 and then inflated to FY90. The AMDF price is assumed to be in FY89 constant dollars.

ITEM	FY88 COST	FY89-AMDF COST	INFL TO FY90	FY90 COST
Gasket Tube	\$1.5 0	\$39.74/1.3=\$30.57	1.0774	\$1.62 \$31.67
Contact	\$11.38		1.0774	\$12.26
Resistor Cap-Plug			1.0774 1.0774	#36.51 #0.98

8. See attached detail sheet for roll-up of repair parts costs.

INRGER - PEPLENISHMENT REPRIR PARTS DETAIL	בר בר בר
PAPT	1
REPRIR	רניים כי
SHEENT	121
PEPLENI	1 + 1 1
1	ī
M257 DISCHIRGER	1200
M257	

	FY91	FY92	FY93	FY94	COST ELEMENT FY95	NT 5.011 FY96	FY90 CONSTANT DOLLARS FY97 FY98 F	TANT DOLL	FRS FY99	FY00-11
DISCHARGER PRODUCT'N	1250	1250	1250	1250	1250	1250	1250	1250		~
ACTIVE CURNTITY	1175	1175	1175	1175	1175	1175	1175	1175		6
1% FOR MAIN FLOAT 95% ACTIVITY RATE	·									-9
H257 DISCHRRGER FIELDED GURNTITIES		1175	2350	3525	4700	5875	7050	8225	9400	9400
REPLENISHMENT REPRIR PARTS GRSKET X .005 X UNIT CST X INFL FAC	.	5.8750 1.50 1.0774	11.7500 1.50 1.0774	17.6250 1.50 1.0774	23.5000 1.50 1.0774	29.3750 1.50 1.0774	35.2500 1.50 1.0774	41.1250 1.50 1.0774	47.0000 1.50 1.0774	FY00-11 (12 years 47.0000 1.50
GRSKET COST		9.5	19.0		38.0	47.5	57.0	66.5	76.0	911.5
TUBE X .005 X UNIT CST		5.8750	7500	17.6250 31.67	23.5000	29.3750 31.67	35.2500 31.67	41.1250	47.0000 31.67	47.0000 31.67
TUBE COST	٠	186.1	372.1	558.2	744.2	930.3	1116.4	1302.4	1489.5	17861.9
ELECT CONT X .015 X UNIT CST X INFL FAC	-	28 SG 1	35.2500 11.38 1.0774	52.8750 11.38 1.0774	70.5000 11.38 1.0774	98.1250 11.38 1.0774	105,7500 11,38 1,0774	123.3750 11.38 1.0774	141.0000 11.38 1.0774	141.0000 11.38 1.0774
ELECTRICAL CONT COST		٠.		1 1	864.4	1080.5	1296.6	1512.7	1728.8	20745.3
RESISTR NETHK X .005 X UNIT CST X INFL FAC	·		11.7500 33.89 1.0774	17.6250 33.89 1.0774	23.5000 33.89 1.0774	29.3750 33.89 1.0774	35.2500 33.89 1.0774	41.1250 33.89 1.0774	47.0000 33.89 1.0774	47.0000 33.89 1.0774
RESISTOR NETWRK COST		-	•	643.5		1072.6	1287.1	1501.6	1716.1	20593.4
CAP-PLUG X 2.47 X UNIT CST X INFL FRC		25	5804.50 0.91 1.0774	8706.75 0.91 1.0774	11609.00 0.91 1.0774	14511.25 0.91 1.0774	l i	0315.75 0.91 1.0774	23218.00 0.91 1.0774	23218.00 0.91 1.0774
CAP PLUG COST		2845.5	5690.9	8536.4	11391.9	14227.3	17072.8	19918.3	22763.7	273164.6
TOTAL REPAIR PARTS		3471.6	6943.3	10414.9	13886.5	17358.2	20829.8	24301.4	27773.1	333276.6

M257 DISCHARGER - REPLENISHMENT REPRIP PARTS DETAIL COST ELEMENT 5.011-FY90 CONSTANT DOLLARS

34575.5 29769.8 1519.1 34322.3 2845.5 455274.3 3471.6 555461.1 TOTAL 9.5 1.50 1.0774 **5.87**50 33.89 214.5 31.67 186.1 1.0774 11.38 216.1 1.0774 2902.25 0.91 5.8750 5.8750 17.6250 1.0774 2350 11.7500 31.67 33.88 1.50 11.38 432.2 1.0774 429.0 5804.50 0.91 11,7500 19.0 35.2500 1.0774 372.1 6943.3 1.0774 11.7500 1.0774 5690.9 FY17 23.5000 -17.6250 33.89 33.89 1.0774 1.0774 17.6250 1.50 1.0774 17.6250 31.67 52.6750 11.38 1.0774 8706.75 0.91 3525 28.5 1.0774 558.2 648.3 643.5 TOTAL REPRIR PRRTS 24301.4 20829.8 17358.2 13886.5 10414.9 8536.4 23.5000 31.67 70.5000 11.38 1.0774 1.50 4700 23.5000 38.0 744.2 864.4 20315.75 17413.50 14511.25 11609.00 0.91 0.91 0.91 0.91 858.1 1.0774 17072.8 14227.3 11381.9 FY15 29.3750 31.67 29,3750 88.1250 11.38 1.0774 5875 47.5 29.3750 33.89 1.0774 1.50 930.3 1072.6 1.0774 1080.5 1.0774 FY14 123.3750 105.7500 11.38 11.38 1.0774 1.0774 35.2500 31.67 35.2500 33.89 1.0774 7050 35,2500 1.50 57.0 1.0774 1116.4 1296.6 1287.1 1.0774 FYI3 19918.3 41.1250 11.1250 1.50 66.5 RESISTR NETWK X .005 41.1250 X UNIT CST 33.89 X INFL FRC 1.0774 1.0774 8225 1.0774 1302.4 1512.7 RESISTOR NETWRK COST 1501.6 FY12 DISCHARGER PRODUCT'N GRSKET X .005

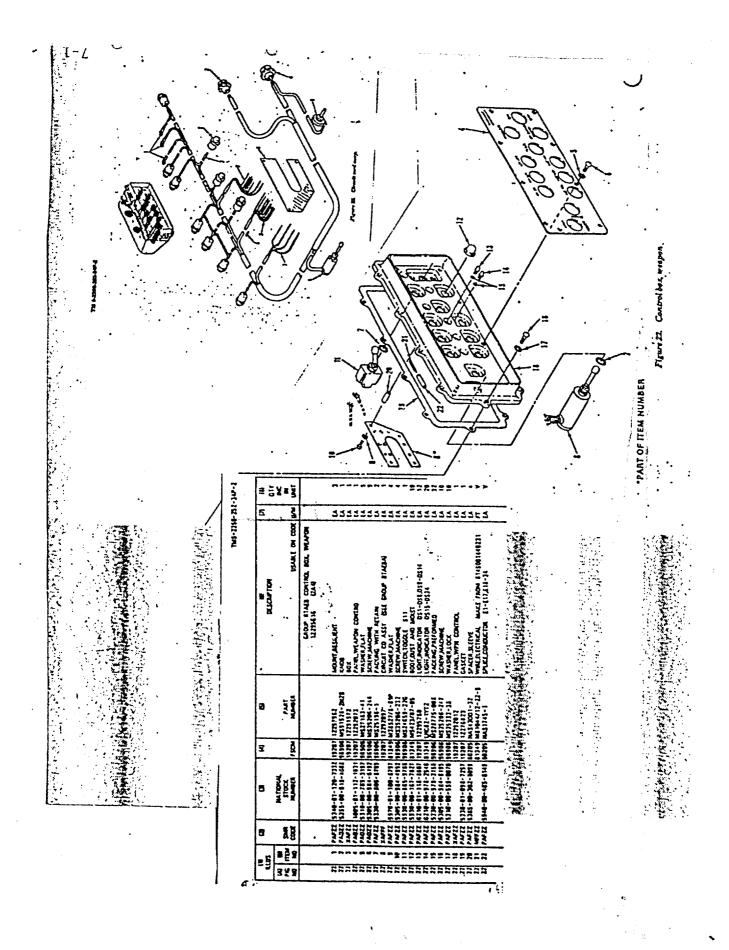
CRSKET X .005

X UNIT CST

X INFL FRC ELECTRICAL CONT COST X UNIT CST X INFL FAC X UNIT CST CHP-PLUG X 2.47 X UNIT CST X INFL FRC FIELDED OURNTITIES 12 FOR MIN FLOMT 95% ACTIVITY RATE ELECT CONT X .015 REPLBNISHMENT ACTIVE CLANTITY H257 DISCHARGER GRSKET COST TURE COST CRP PLUG COST x 29. TUBE X .005

Replenishment of Repair

Parts Data



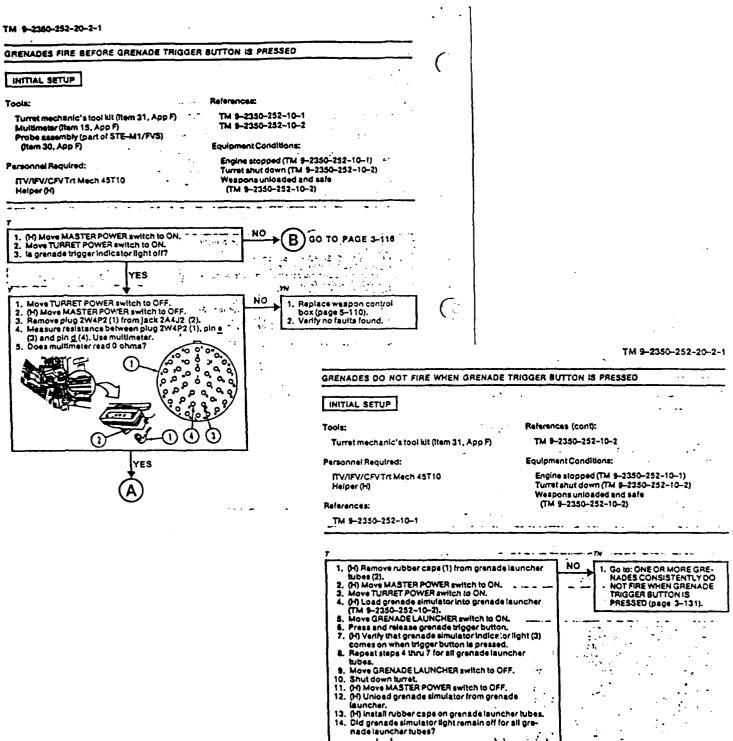
ANNEX 7 - BFV Integration Data

BEST AVAILABLE COPY

TM 9-2350-252-20-2-1

GRENADE LAUNCHER SYSTEM FAULT SYMPTOM INDEX

en de la companya della companya della companya de la companya della companya de	FAULT SYMPTOM
GRENADE LAUNCHER SY	STEM HAS SOMETHING WRONG
Section 4 - Par Section 1 - Section 1 - Se	
_GRENADES DO NOT FIRE	WHEN GRENADE TRIGGER BUTTON IS PRESSED
GRENADES FIRE BEFORE	GRENADE TRIGGER BUTTON IS PRESSED
GRENADE LAUNCHER OR	TRIGGER INDICATOR LAMP DOES NOT COME
GRENADE LAUNCHER OR	TRIGGER INDICATOR LIGHT DOES NOT GO OFF
ONE OR MORE GRENADE	S CONSISTENTLY DO NOT FIRE WHEN GRENADE
GRENADE LAUNCHER SY	STEM INTERCONNECTION TABLE



Trools: Terror rechanis's leel bit flows 31, App P) Multimoster (him 16, App P) To 4-330-332-10-1 Multimoster (him 16, App P) Personnel Requires: Engine stopped (TM 9-2330-232-10-1) Turret shrut down (TM 9-2330-132-10-2) Wespons unfoesded and table (TV/PV/CVT/TI Mech 45T10 Multimoster (him 16, App P) 1. Op More MASTER POWER pristicn to ON. 2. Move TURRET POWER pristicn to ON. 3. Move TURRET POWER pristicn to ON. 4. Obesi granded suncher trigger indicator Signi come on? VES ONE OR MORE GRENADES CONSISTENTLY DO NOT FIRE WHEN 0 IS PRESSED. INITIAL SETUP Tools: ONE OR MORE GRENADES CONSISTENTLY DO NOT FIRE WHEN 0 IS PRESSED. INITIAL SETUP Tools: Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanic's tool NII (term 31, App P) The 3-230-232-1 Turrit mechanics tool NII (term 31, App P) The 3-230-232-1 Turrit mechanics tool NII (term 31, App P) The 3-230-232-1 The 3-230-232-1 Turrit mechanics tool NII (term 31, App P) The	echanic's tool kit (from 31, App P) for (from 18, App P) asembly (part of \$15-M1/FVS) 0, App P) Required:	Reference TM 9-1 TM 9-2 TM 9-2 Equipmer Engine Weapon (TM 9	ME: 1150-252-10-1 1150-252-10-2 ME Conditional 1270-004 (That 3-22) 1284 down (That 3-22) 1280-252-10-29	50-232-10-1) 250-232-10-2)
Tools: Turbut rechanie's teel int (teen 31, App 9) Multimater (than 16, App 9) The 3230-132-10-1 This 3230-132-10-1 Turbut intuit down (TM 9-2330-132-10-1) Turbut intuit intu	echanic's tool lik (fem 31, App P) to (fem 18, App P) Required: CPVTrr, Mech 43T10 H) TO MASTER POWER switch to ON. TO MERET POWER switch to ON. TO Grand launcher indicator light co	TM 8-7 TM 8-2 Equipment Engine Turnet: Weapo (TM 8	ME: 1250-252-10-1 1250-252-10-2 In Conditional Proposed (TM 9-22) and down (TM 9-22)	50-252-10-1) 350-252-10-7) ale
Turnet inschanle's teal int (flein 31, App 8) Multimater (flein 16, App 9) The +3350-321-0-1 The +3350-321-0-2 The +3350-321-0-2 The +3350-321-0-2 The +3350-321-0-1 The +3350-32	ter (flam 18, App P) seembly (part of STE-M1/FVS) 0, App P) Required: CFVTrt Mech 45T10 M) are MASTER POWER switch to ON. 1, TURRET POWER switch to ON. 1, TURRET POWER switch to ON. 1, granade (suncher indicator light co	TM 8-7 TM 8-2 Equipment Engine Turnet: Weapo (TM 8	ME: 1250-252-10-1 1250-252-10-2 In Conditional Proposed (TM 9-22) and down (TM 9-22)	50-252-10-1) 350-252-10-7) ale
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TUTRY INCOMPTA Mech 45T10 Tutret shut down (TM 9-2330-232-10-2) Wespons unleased and tallo (TM 9-2330-232-10-2) I. PO More NAUSTER POWER switch to ON. 2. Move TURRET POWER switch to ON. 3. Down TURRET POWER switch to ON. 4. Move TURRET POWER switch to ON. 5. Down prinade isuncher indicate light come on? 1. Move FANALAMP TEST switch to LAMP TEST post- 2. Down prinade isuncher indiges indicate light come 2. Down prinade isuncher indiges indicate light come 3. Down MASTER POWER 2. Switch to OFF. 3. Replace we spon- sentral 4. Work you is said found. 4. Work you is said found. A Sepace we spon- sentral 5. PRESSED Turret mechanic's tool VII (terra) 11. App P) Tools Turret mechanic's tool VII (terra) 12. App P) Turret shut down Farmons (TV/FY/CPYTri Mech 43T12) 8. Replace we spon- 8. Repose we spon- 8. Repose we spon- 8. Switch to OFF. 9. Mellon 13. App P) Turret shut down 1. Move TURRET POWER 9. Switch to OFF. 9. Mellon 13. App P) Turret shut down 1. Presonand Requires: Equipment Condition 1. Po Remove rupber caps (1) from grenade isuncher 1. Do Remove rupber caps (1) from grenade isuncher 1. Do Nove MASTER POWER switch to ON. 4. Mever TURRET POWER switch to ON. 5. Mever QRENADE LUNCHER switch to ON. 6. Press granade isuncher folicits on grenade isuncher (1) appended to one of the origin o	CPVTrt Mech 43T10 H) ere MASTER POWER purish to ON. TURRET POWER to Which to ON. granade launcher Widicator light co YES s and release grenade launcher trigo	Turret: Wezpo	shut down (TM \$-2: ms unloaded and a: h-2350-252-10-2)	350-252-10-71 ale
1. 09 Move MASTER POWER syntchie ON. 2. Move TURRET POWER syntchie ON. 3. Move GRANDE LAUNCHER syntch to ON. 4. Does grandel leuncher indicator light come on? VES 1. Move FANZAMP TEST syntch to LUMP TEST position. Son. 2. Did granade isuncher bigger indicator light come. 3. Did granade isuncher bigger indicator light come. 3. Replace was pen centrol box (sage 3-10). 4. Verify no faulta found. INITIAL SETUP Tools: Turnst machanic's tool Nt (flem 31, App P) The Passances (conft: Turnst machanic's tool Nt (flem 31, App P) The Passances (conft: Turnst machanic's tool Nt (flem 31, App P) The Passances (conft: Turnst should gern confidences: The Passances (conft: Turnst should gern conft: Turnst should gern confidences: The Passances (conft: The Passances (FTURRET POWER switch to ONL I granade (suncher Indicator light co YES s and release grenade (suncher trigo			
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Son. 2. Did grenade launcher brigger indicator light come on? 2. Did grenade launcher brigger indicator light come on? 3. Replace weapon centrol box (bages 3-110). 4. Verity ne lauta feund. GO TO NEXT PAGE GHE OR MORE GRENADES CONSISTENTLY DO NOT FIRE WHEN Q IS PRESSED INITIAL SETUP Tools: Torrel mechanic's tool Nil (tiem 31, App P) The P-23Ju-252-1 Parsonnel Required: Equipment Consistent ITV/FV/CPVTrt Mech 43T13 Engine stopped (There is an indicator) References: TM 9-23J0-252 T	a and release grenade launcher trig: s grenade launcher trig; per indicator		# \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	
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GO TO NEXT PAGE OHE OR MORE GRENADES CONSISTENTLY DO NOT FIRE WHEN O IS PRESSED INITIAL SETUP Toolic Recommended to soot kill (term 31, App P) The P3334-232-1 Personnel Required: Equipment Constitution ITVARVICEY In Mech 49713 Engine atapped (Thurst shut deem) Wespons unloade References: (The P-2330-232 TM 9-2330-252-10-1 P 1. 09 Remove rubber cape (1) from granade launcher side (2). 2. 09 Land granade simulator (3) in granade launcher side (3). 3. 09 Lines of granade simulator (3) in granade launcher side (3). 4. Meve of RANASTER POWER switch to ONL 4. Meve OR RANGE LAUNCHER switch to ONL 5. Meve OR RANGE LAUNCHER switch to ONL 6. Fros granade simulator (3) on granade simulator (3) 8. 09 Meves granade simulator (7) to next granade Buscher Value (3).	YES	.,		
OME OR MORE GRENADES CONSISTENTLY DO NOT FIRE WHEN O IS PRESSED INITIAL SETUP Tools: References (cond: Turns mechanic's tool til (tem 31, App P) Personnel Required: Equipment Condition ITV/FV/CPVTrt Mech 43713 Engine stopped (T Helper (H) Turns shut dewn) Wespons unloade References: (TM 9-2330-232 TM 9-2330-232-10-1 P 1. 09 Remove rubber caps (1) from grenade launcher bibes (T). 2. 09 Last grenade simulator (3) in grenade launcher bibes (T). 3. 09 Memove Turnster Powers meticn to Ont. 4. Meyer Turnster Powers meticn to Ont. 6. Meyer Granade Launcher trigger (s). 7. Memove grenade simulator (7) to next grenade B. 09 Meyer grenade simulator (7) to next grenade B. 09 Meyer grenade simulator (7) to next grenade Buscher (top) (2) on grenade simulator (3) B. 09 Meyer grenade simulator (7) to next grenade				
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S. Mave GRENADE LAUNCHER switch to On. 6. Press grenade aleuncher trigger (s). 7. 09 Check whether light (3) on grenade simulator (1) semas en. 8. 09 Neve grenade simulator (2) to next grenade liturcher tribe (7).		· ·		
9. Repeat steps 4 linu 8 above until alt granade lisuncher bubs (2) have been checked. 10. (b) Venhy In at liquit on granade simulator comes on for each granade bubs (fred but alto fred but at liquid but at liq			3 3	
printed a function to be a write us OA Form 2404 and faulty granded a function. 77. Report practical to supervisor.				